

Systems Analysis and Control

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Lecture 6: Calculating the Transfer Function

Introduction

In this Lecture, you will learn: Transfer Functions

- Transfer Function Representation of a System
- State-Space to Transfer Function
- Direct Calculation of Transfer Functions

Block Diagram Algebra

- Modeling in the Frequency Domain
- Reducing Block Diagrams

Previously:

The Laplace Transform of a Signal

Definition: We defined the Laplace transform of a **Signal**.

- **Input**, $\hat{u} = \mathcal{L}(u)$.
- **Output**, $\hat{y} = \mathcal{L}(y)$

Theorem 1.

Any bounded, linear, causal, time-invariant system, G , has a **Transfer Function**, \hat{G} , so that if $y = Gu$, then

$$\hat{y}(s) = \hat{G}(s)\hat{u}(s)$$

There are several ways of finding the *Transfer Function*.

Transfer Functions

Example: Simple System

State-Space:

$$\begin{aligned}\dot{x}(t) &= -x(t) + u(t) \\ y(t) &= x(t) - .5u(t) \quad x(0) = 0\end{aligned}$$

Apply the Laplace transform to the first equation:

$$\mathcal{L}\left(\dot{x}(t) = -x(t) + u(t)\right) \quad \text{which gives} \quad s\hat{x}(s) = -\hat{x}(s) + \hat{u}(s).$$

Solving for $\hat{x}(s)$, we get

$$(s + 1)\hat{x}(s) = \hat{u}(s) \quad \text{and so} \quad \hat{x}(s) = \frac{1}{s + 1}\hat{u}(s).$$

Similarly, the second equation yields:

$$\hat{y}(s) = \hat{x}(s) - .5\hat{u}(s) = \frac{1}{s + 1}\hat{u}(s) - .5\hat{u}(s) = \frac{1 - .5(s + 1)}{s + 1}\hat{u}(s) = \frac{1}{2} \frac{s - 1}{s + 1}\hat{u}(s)$$

Thus we have the **Transfer Function**:

$$\hat{G}(s) = \frac{1}{2} \frac{s - 1}{s + 1}$$

Transfer Functions

Example: Step Response

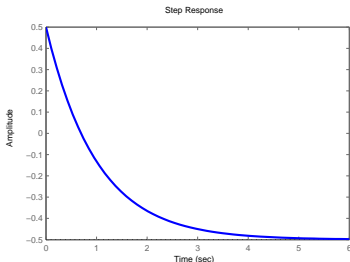
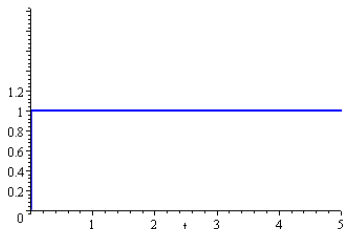
The *Transfer Function* provides a convenient way to find the response to inputs.

Step Input Response: $\hat{u}(s) = \frac{1}{s}$

$$\begin{aligned}\hat{y}(s) &= \hat{G}(s)\hat{u}(s) = \frac{1}{2} \frac{s-1}{s+1} \frac{1}{s} = \frac{1}{2} \frac{s-1}{s^2+s} \\ &= \frac{1}{2} \left(\frac{2}{s+1} - \frac{1}{s} \right)\end{aligned}$$

Consulting our table of Laplace Transforms,

$$\begin{aligned}y(t) &= \frac{1}{2} \mathcal{L}^{-1} \frac{2}{s+1} - \frac{1}{2} \mathcal{L}^{-1} \frac{1}{s} \\ &= e^{-t} - \frac{1}{2} \mathbf{1}(t)\end{aligned}$$



Transfer Functions

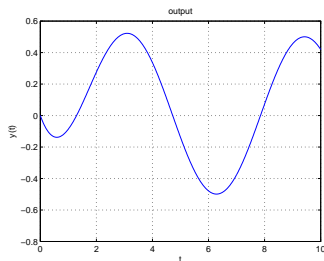
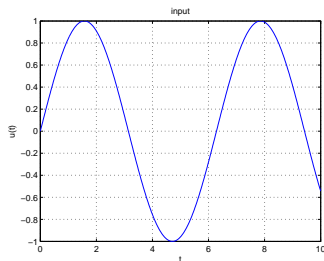
Example: Sinusoid Response

Sine Function: $\hat{u}(s) = \frac{1}{s^2+1}$

$$\begin{aligned}\hat{y}(s) &= \hat{G}(s)\hat{u}(s) = \frac{1}{2} \frac{s-1}{s+1} \frac{1}{s^2+1} \\ &= \frac{1}{2} \frac{s-1}{s^3+s^2+s+1} \\ &= \frac{1}{2} \left(\frac{s}{s^2+1} - \frac{1}{s+1} \right)\end{aligned}$$

Consulting our table of Laplace Transforms,

$$y(t) = \frac{1}{2} \cos t - \frac{1}{2} e^{-t}$$



Note that this is the same answer we got by integration in Lecture 4.

Inverted Pendulum Example

Return to the pendulum.

Dynamics:

$$\ddot{\theta}(t) = \frac{Mgl}{2J}\theta(t) + \frac{1}{J}T(t)$$

$$y(t) = \theta(t)$$

For the first equation,

$$s^2\hat{\theta}(s) = \frac{Mgl}{2J}\hat{\theta}(s) + \frac{1}{J}\hat{T}(s)$$

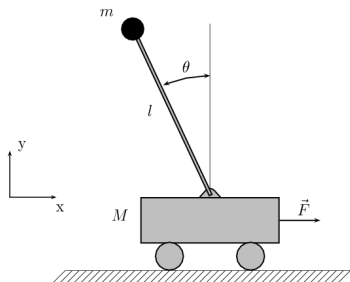
Solve for $\hat{\theta}(s)$:

$$\hat{\theta}(s) = \frac{1}{J} \frac{1}{s^2 - \frac{Mgl}{2J}} \hat{T}(s)$$

Second Equation: $\hat{y}(s) = \hat{\theta}(s)$

Transfer Function:

$$\hat{G}(s) = \frac{\hat{y}(s)}{\hat{T}(s)} = \frac{1}{J} \frac{1}{s^2 - \frac{Mgl}{2J}}$$



Inverted Pendulum Example: Impulse Response

Impulse Input: $\hat{u}(s) = 1$

$$\begin{aligned}\hat{y}(s) &= \hat{G}(s)\hat{u}(s) = \frac{1}{J} \frac{1}{s^2 - \frac{Mgl}{2J}} \\ &= \frac{1}{J} \frac{1}{\left(s - \sqrt{\frac{Mgl}{2J}}\right)\left(s + \sqrt{\frac{Mgl}{2J}}\right)} \\ &= \frac{1}{J} \sqrt{\frac{2J}{Mgl}} \left(\frac{1}{s - \sqrt{\frac{Mgl}{2J}}} - \frac{1}{s + \sqrt{\frac{Mgl}{2J}}} \right)\end{aligned}$$

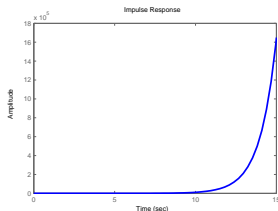


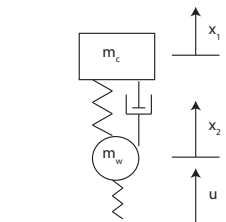
Figure: Impulse Response with $g = l = J = 1, M = 2$

In time-domain:

$$y(t) = \frac{1}{J} \sqrt{\frac{2J}{Mgl}} \left(e^{\sqrt{\frac{Mgl}{2J}}t} - e^{-\sqrt{\frac{Mgl}{2J}}t} \right)$$

Pendulum Accelerates to infinity!

Constructing the Transfer Function: Suspension System



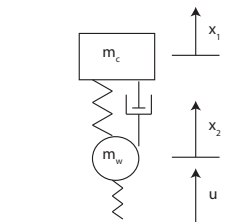
Recall the dynamics:

$$\ddot{z}_1(t) = -\frac{K_1}{m_c} z_1(t) - \frac{c}{m_c} \dot{z}_1(t) + \frac{K_1}{m_c} z_2(t) + \frac{c}{m_c} \dot{z}_2(t)$$

$$\ddot{z}_4(t) = \frac{K_1}{m_w} z_1(t) + \frac{c}{m_w} \dot{z}_1(t) - \left(\frac{K_1}{m_w} + \frac{K_2}{m_w} \right) z_2(t) - \frac{c}{m_w} \dot{z}_2(t) - \frac{K_2}{m_w} u(t)$$

$$y(t) = [z_2(t)]$$

Constructing the Transfer Function: Suspension System



Apply the Laplace Transform to the dynamics:

$$s^2 \hat{z}_1(s) = -\frac{K_1}{m_c} \hat{z}_1(s) - \frac{c}{m_c} s \hat{z}_1(s) + \frac{K_1}{m_c} \hat{z}_2(s) + \frac{c}{m_c} s \hat{z}_2(s)$$

$$s^2 \hat{z}_2(s) = \frac{K_1}{m_w} \hat{z}_1(s) + \frac{c}{m_w} s \hat{z}_1(s) - \left(\frac{K_1}{m_w} + \frac{K_2}{m_w} \right) \hat{z}_2(s) - \frac{c}{m_w} s \hat{z}_2(s) - \frac{K_2}{m_w} \hat{u}(s)$$

$$\hat{y}(s) = \hat{z}_2(s)$$

Constructing the Transfer Function: Suspension System

We isolate the z_1 and z_2 terms:

$$\begin{aligned}\left(s^2 + \frac{c}{m_c}s + \frac{K_1}{m_c}\right) \hat{z}_1(s) &= \left(\frac{K_1}{m_c} + \frac{c}{m_c}s\right) \hat{z}_2(s) \\ \left(s^2 + \frac{c}{m_w}s + \frac{K_1}{m_w} + \frac{K_2}{m_w}\right) \hat{z}_2(s) &= \left(\frac{K_1}{m_w} + \frac{c}{m_w}s\right) \hat{z}_1(s) - \frac{K_2}{m_w} \hat{u}(s) \\ \hat{y}(s) &= \hat{z}_2(s)\end{aligned}$$

Which yields

$$\begin{aligned}\hat{z}_1(s) &= \frac{\left(\frac{K_1}{m_c} + \frac{c}{m_c}s\right)}{\left(s^2 + \frac{c}{m_c}s + \frac{K_1}{m_c}\right)} \hat{z}_2(s) \\ \hat{z}_2(s) &= \frac{\frac{K_1}{m_w} + \frac{c}{m_w}s}{s^2 + \frac{c}{m_w}s + \frac{K_1}{m_w} + \frac{K_2}{m_w}} \hat{z}_1(s) - \frac{\frac{K_2}{m_w}}{s^2 + \frac{c}{m_w}s + \frac{K_1}{m_w} + \frac{K_2}{m_w}} \hat{u}(s)\end{aligned}$$

Constructing the Transfer Function: Suspension System

Now we can plug in for \hat{z}_1 and solve for \hat{z}_2 :

$$\hat{z}_2(s) = \frac{K_2(m_c s^2 + cs + K_1)}{m_c m_w s^4 + c(m_w + m_c)s^3 + (K_1 m_c + K_1 m_w + K_2 m_c)s^2 + cK_2 s + K_1 K_2} \hat{u}(s)$$

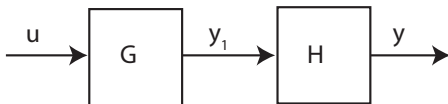
Compare to the State-Space Representation:

$$\frac{d}{dt} \begin{bmatrix} z_1 \\ z_2 \\ z_3 \\ z_4 \end{bmatrix} (t) = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -\frac{K_1}{m_c} & -\frac{c}{m_c} & \frac{K_1}{m_c} & \frac{c}{m_c} \\ 0 & 0 & 0 & 1 \\ \frac{K_1}{m_w} & \frac{c}{m_w} & -\left(\frac{K_1}{m_w} + \frac{K_2}{m_w}\right) & -\frac{c}{m_w} \end{bmatrix} \begin{bmatrix} z_1 \\ z_2 \\ z_3 \\ z_4 \end{bmatrix} (t) + \begin{bmatrix} 0 \\ 0 \\ 0 \\ -\frac{K_2}{m_w} \end{bmatrix} u(t)$$
$$y(t) = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} z_1 \\ z_2 \\ z_3 \\ z_4 \end{bmatrix} (t) + \begin{bmatrix} 0 \\ 0 \end{bmatrix} u(t)$$

Block Diagram Algebra

Series (Cascade) Interconnection

The interconnection of systems can be represented by block diagrams.



Cascade of Systems: Suppose we have two systems: G and H .

Definition 2.

The **Cascade** or **Series** interconnection of two systems is

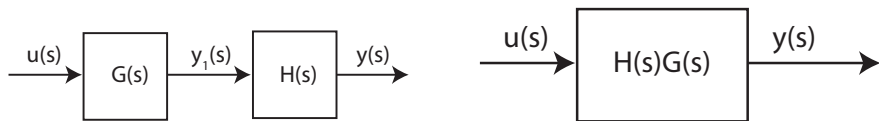
$$y_1 = Gu \quad y = Hy_1$$

or

$$y = H(G(u))$$

Block Diagram Algebra

Series Connection (Cascade)



Series Interconnection:

- The output of G is the input to H .
- Let $\hat{G}(s)$ and $\hat{H}(s)$ be the transfer functions for G and H .
- Then

$$\hat{y}_1(s) = \hat{G}(s)\hat{u}(s) \quad \hat{y}(s) = \hat{H}(s)\hat{y}_1(s) = \hat{H}(s)\hat{G}(s)\hat{u}(s)$$

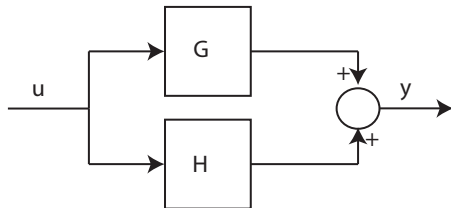
- The *Transfer Function*, $\hat{T}(s)$ for the combination of G and H is

$$\hat{T}(s) = \hat{H}(s)\hat{G}(s)$$

Note: The order of the \hat{G} and \hat{H} !

Block Diagrams

Parallel Connection



Parallel Interconnection: Suppose we have two systems: G and H .

Definition 3.

The **Parallel** interconnection of two systems is

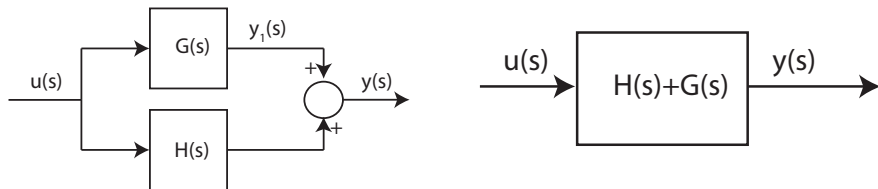
$$y_1 = Gu \quad y_2 = Hu \quad y = y_1 + y_2$$

or

$$y = H(u) + G(u)$$

Block Diagrams

Parallel Connection



The Transfer function of a Parallel interconnection:

- Laplace transform:

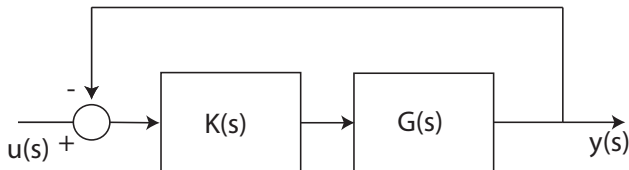
$$\hat{y}(s) = \hat{y}_1(s) + \hat{y}_2(s) = \hat{G}(s)\hat{u}(s) + \hat{H}(s)\hat{u}(s) = \left(\hat{H}(s) + \hat{G}(s)\right)\hat{u}(s)$$

- The *Transfer Function*, $\hat{T}(s)$ for the parallel interconnection of G and H is

$$\hat{T}(s) = \hat{H}(s) + \hat{G}(s)$$

Block Diagrams

Lower Feedback Interconnection



Feedback:

- **Controller:** $z = K(u - y)$ **Plant:** $y = Gz$

In the Frequency Domain:

$$\hat{z}(s) = -\hat{K}(s)\hat{y}(s) + \hat{K}(s)\hat{u}(s) \qquad \hat{y}(s) = \hat{G}(s)\hat{z}(s)$$

so

$$\hat{y}(s) = \hat{G}(s)\hat{z}(s) = -\hat{G}(s)\hat{K}(s)\hat{y}(s) + \hat{G}(s)\hat{K}(s)\hat{u}(s)$$

Solving for $\hat{y}(s)$,

$$\hat{y}(s) = \frac{\hat{G}(s)\hat{K}(s)}{1 + \hat{G}(s)\hat{K}(s)}\hat{u}(s)$$

Block Diagrams

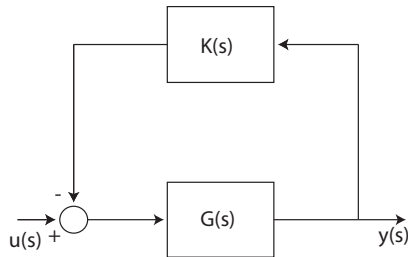
Upper Feedback Interconnection (Regulators)

There is another Feedback interconnection

- u is the input
- y is the output

$$\hat{y}(s) = \hat{G}(s)\hat{z}(s)$$

$$\hat{z}(s) = u(s) - \hat{K}(s)\hat{y}(s)$$



Which yields

$$\hat{y}(s) = \hat{G}(s) \left(u(s) - \hat{K}(s)\hat{y}(s) \right) = \hat{G}(s)\hat{u}(s) - \hat{G}(s)\hat{K}(s)\hat{y}(s)$$

hence the Transfer Function is:

$$\hat{y}(s) = \frac{\hat{G}(s)}{1 + \hat{G}(s)\hat{K}(s)}\hat{u}(s).$$

The Effect of Feedback: Impulse Response

Inverted Pendulum Model

Transfer Function

$$\hat{G}(s) = \frac{1}{Js^2 - \frac{Mgl}{2}}$$

Controller: Static Gain: $\hat{K}(s) = K$

Input: Impulse: $\hat{u}(s) = 1$.

Closed Loop: Lower Feedback

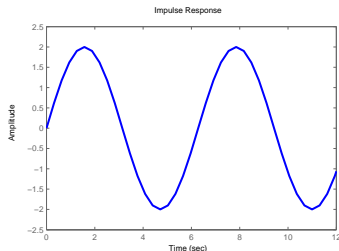
$$\hat{y}(s) = \frac{\hat{G}(s)\hat{K}(s)}{1 + \hat{G}(s)\hat{K}(s)}\hat{u}(s) = \frac{\frac{K}{Js^2 - \frac{Mgl}{2}}}{1 + \frac{K}{Js^2 - \frac{Mgl}{2}}} = \frac{K}{Js^2 - \frac{Mgl}{2} + K}$$

First Case:

- If $K > \frac{Mgl}{2}$, then $K - \frac{Mgl}{2} > 0$, so

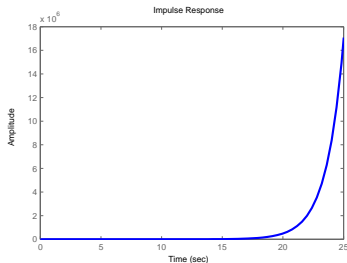
$$\hat{y}(s) = \frac{K/J}{s^2 + \left(K/J - \frac{Mgl}{2J}\right)}$$

$$y(t) = \frac{K}{J\sqrt{K/J - \frac{Mgl}{2J}}} \sin\left(\sqrt{K/J - \frac{Mgl}{2J}}t\right)$$



The Effect of Feedback: Impulse Response

Inverted Pendulum Model



Second Case:

- If $K < \frac{Mgl}{2}$, then $K - \frac{Mgl}{2} < 0$, so

$$\hat{y}(s) = \frac{K}{J} \left(\frac{1}{s - \sqrt{K/J - \frac{Mgl}{2J}}} + \frac{1}{s + \sqrt{K/J - \frac{Mgl}{2J}}} \right)$$

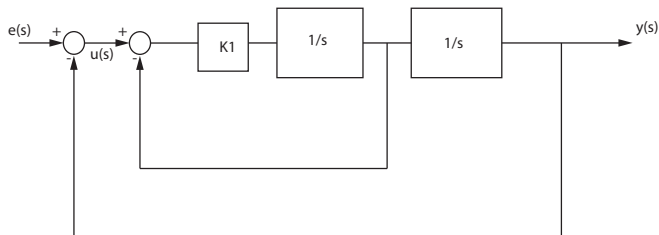
$$y(t) = \frac{K}{J} \left(e^{\sqrt{K/J - \frac{Mgl}{2J}}t} + e^{-\sqrt{K/J - \frac{Mgl}{2J}}t} \right)$$

Important: Value of K determines stability vs. instability

Block Diagrams

Reduction

Now let's look at how to reduce a more complicated interconnections



Label

- The output from the inner loop z
- The input to the inner loop u

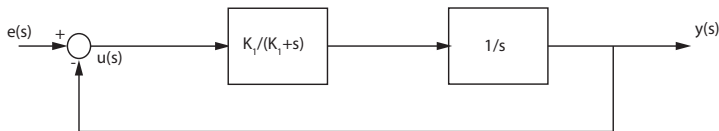
First **Close the Inner Loop** using the *Lower Feedback Interconnection*.

$$\hat{z}(s) = \frac{\frac{K_1}{s}}{\frac{K_1}{s} + 1} \hat{u}(s) = \frac{K_1}{K_1 + s} \hat{u}(s)$$

Block Diagrams

Reduction

We now have a reduced Block Diagram



Again, apply the *Lower Feedback Interconnection*:

$$\hat{y}(s) = \frac{\frac{K_1}{s(K_1+s)}}{1 + \frac{K_1}{s(K_1+s)}} \hat{e}(s) = \frac{K_1}{s(K_1+s) + K_1} \hat{e}(s)$$

So the Transfer function is $\hat{T}(s) = \frac{K_1}{s^2 + K_1s + K_1}$

Summary

What have we learned today?

Transfer Functions

- Transfer Function Representation of a System
- State-Space to Transfer Function
- Direct Calculation of Transfer Functions

Block Diagram Algebra

- Modeling in the Frequency Domain
- Reducing Block Diagrams

Next Lecture: Partial Fraction Expansion